

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
24 April 2003 (24.04.2003)

PCT

(10) International Publication Number
WO 03/033558 A2

(51) International Patent Classification⁷: C08F 222/10,
G02B 1/04

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(21) International Application Number: PCT/EP02/11431

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(22) International Filing Date: 11 October 2002 (11.10.2002)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:
60/329,086 12 October 2001 (12.10.2001) US
60/328,810 15 October 2001 (15.10.2001) US

(81) Designated States (*national*): AE, AG, AL, AM, AT, AU,
AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU,
CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH,
GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC,
LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW,
MX, MZ, NO, NZ, OM, PH, PL, PT, RO, RU, SD, SE, SG,
SI, SK, SL, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ,
VC, VN, YU, ZA, ZM, ZW.

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(84) Designated States (*regional*): ARIPO patent (GH, GM,
KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW),
Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM),
European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE,
ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE, SK,
TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ,
GW, ML, MR, NE, SN, TD, TG).

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Published:

— *without international search report and to be republished
upon receipt of that report*

*For two-letter codes and other abbreviations, refer to the "Guid-
ance Notes on Codes and Abbreviations" appearing at the begin-
ning of each regular issue of the PCT Gazette.*

(54) Title: HIGH INDEX CURABLE PHOTOCHROMIC COMPOSITION AND ITS PROCESS

(57) Abstract: There is provided a high refractive index, curable, synthetic resin composition comprising a core resin composition composed of a mixture of ethylenically unsaturated compounds, and an initiation system containing both photo and thermal initiators, particularly a photochromic resin composition which further includes at least one photochromic dye. There is also provided a curing process, which includes a combination of multi-step radiation curing a thermal annealing. Articles produced of the cured composition exhibit superior physical and, in appropriate cases, photochromic properties and can be easily mass produced on a commercial scale due to short processing time and use of readily available chemicals.

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HIGH INDEX CURABLE PHOTOCHROMIC COMPOSITION AND ITS PROCESS

The present invention relates to a high refractive index curable synthetic resin composition, a process for curing such a composition, and a cured article formed thereof.

Currently, commercial photochromic plastic lenses with photochromic dyes dispersed throughout the lens substrate are made by thermal processes. These processes yield product with good mechanical, optical and photochromic properties, but they require normally around 20 hours before the curing is complete. Examples of such thermally cured lenses are disclosed in U.S. Patent No. 5,763,511, to Chan et al.; U.S. Patent No. 5,973,039, to Florent et al.; and U.S. Patent No. 6,034,193, to Henry et al.

Attempts have also been made to produce synthetic resin lenses by radiation curing. Examples of such attempts to produce radiation cured lenses are described in U.S. Patent No. 5,621,017, to Kobayakawa et al., and U.S. Patent No. 5,910,516, to Imura et al. Although the use of radiation curing makes it possible to reduce processing time, the resulting lenses have not found successful commercial application due to one or more of the following reasons:

- (1) inferior thermal/mechanical properties,
- (2) poor optical and/or photochromic properties, and
- (3) lack of commercial capability for mass production.

Thus, despite the efforts of the prior art to make synthetic resin lenses through radiation curing, there are still no commercial photochromic lenses produced via radiation cure in the market. There has remained a need to solve these problems by finding a proper radiation curable photochromic composition, along with the process to produce superior synthetic resin lenses.

The technical problem underlying the present invention is thus to develop a cur-

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able core resin composition which can be cured rapidly by radiation curing methods and/or thermally to produce synthetic resin lenses with desirable thermal and mechanical properties, good optical characteristics and, in the case of photochromic lenses, photochromic characteristics, and which are capable of mass production on a commercial scale.

The solution to the above technical problem is achieved by the embodiments characterized in the claims.

In particular, the present invention relates to a new curable core resin composition suitable for photochromic dyes, along with a new initiation system containing both photo and thermal initiators. The unique cure process includes combination of both step radiation cure and thermal annealing, leading to lenses with superior physical and/or photochromic properties in as little as one hour.

In a first aspect, the present invention relates to a high refractive index curable synthetic resin composition comprising a core resin composition of ethylenically unsaturated compounds and a photo initiator and a thermal initiator.

In accordance with a further aspect of the present invention the synthetic resin composition further comprises at least one photochromic dye and is suitable for the production of photochromic lenses. The photochromic composition according to the present invention provides superior photochromic properties and physical properties, short processing time through both step radiation and thermal curing, and easy commercial capability for mass production.

The present invention also relates to a radiation curing process of the compositions of the present invention via a single stage cure or via a multiple stage cure with an appropriate cooling period at the end of each cure stage, followed by thermal annealing.

The present invention may be understood more readily by reference to the following detailed description of particular embodiments of the invention and the specific

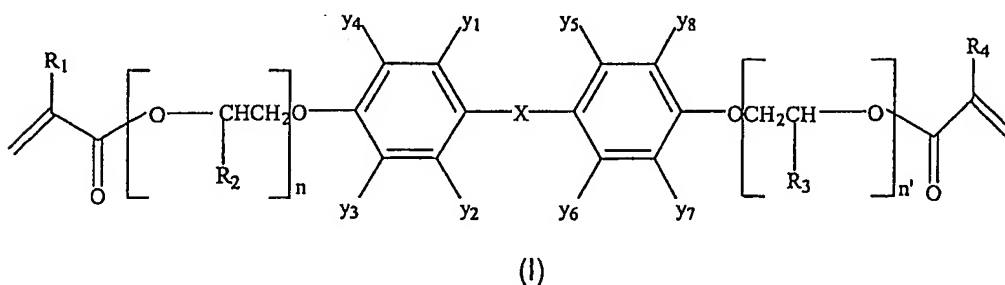
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examples included therein. Before the present compositions and their process are disclosed and described, it is to be understood that this invention is not limited to a particular formulation and a process, as such may, of course, vary. It is also to be understood that the terminology used herein is for the purpose of describing particular embodiments only and is not intended to be limiting. As used herein, the term "(meth)acrylate" is intended to refer generally to both acrylate and methacrylate functional groups.

The present invention relates to a high refractive index curable core resin composition suitable for photochromic application. When proper photochromic dyes, initiation system containing both photo and thermal initiators and additives are incorporated into the composition according to the present invention, lenses with superior physical and photochromic properties can be made through the curing process according to the present invention.

In one aspect, the core resin composition suitable for photochromic application comprises per 100 parts by weight:

(i) from 2 to 70 parts by weight of at least one first compound corresponding to formula (I):



wherein

n and n' independently are 0-30

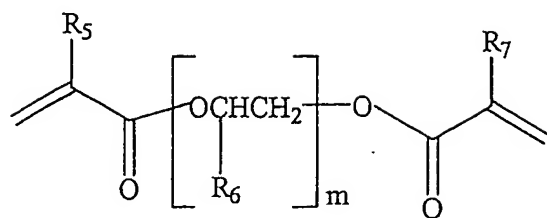
R_1 - R_4 independently represent H or C_1 - C_6 alkyl,

X is O, S, SO_2 , CO_2 , CH_2 , $CH=CH$, $C(CH_3)_2$ or a single bond, and

y_1 - y_8 independently represent H, OH, halogen, mercaptan or C_1 - C_4 alkyl;

(ii) from 2 to 80 parts by weight of at least one second compound corresponding to formula (II):

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(II)

wherein

m is at least 1, and

R₅-R₇ independently represent H or C₁-C₆ alkyl;

(iii) from 2 to 60 parts by weight of a reactive diluent selected from the group consisting of 1,6-hexanediol di(meth)acrylate, isobornyl (meth)acrylate, 2-hydroxyethyl (meth)acrylate, 2-phenoxyethyl (meth)acrylate, vinyl benzoate, vinyl 4-t-butyl benzoate, styrene, divinyl benzene, polyethylene glycol di(meth)acrylate, polypropylene glycol di(meth)acrylate and mixtures thereof; and

(iv) from 2 to 60 parts by weight of a multi-functional (meth)acrylate or (meth)acrylate derivative with three or more acrylate functional groups selected from the group consisting of trimethylolpropane tri(meth)acrylate, pentaerythritol tri(meth)acrylate, glyceryl tri(meth)acrylate, pentaerythritol tetra(meth)acrylate, di-trimethylolpropane tetra(meth)acrylate, dipentaerythritol penta(meth)acrylate, penta(meth)acrylate ester and mixtures thereof.

In preferred compounds of formula I, R₁ and R₄ are CH₃; R₂, R₃, and y₁-y₈ are hydrogen; and X is C(CH₃)₂. n and n' are preferably 3 to 5. In preferred compounds of formula II, R₅ and R₇ are CH₃, and R₆ is hydrogen.

To make a photochromic article, the core resin composition of the present invention may further comprise an effective photochromic amount of at least one photochromic dye incorporated therein to form photochromic lenses which darken when exposed to bright light and fade when under less intense light exposure. Suitable photochromic dyes may, for example, comprise chromenes, fulgides, fulgimides, spirooxazines, naphthopyrans, and/or mixtures thereof. Examples of useful photochromic dye compounds and/or mixtures are disclosed in U.S. Patent Nos. 5,399,687; 5,498,686; 5,623,005; 5,645,768; 5,707,557; 5,801,243; 5,932,725;

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5,952,515; 5,990,305; 6,022,496; 6,036,890; 6,102,543; 6,146,554; 6,171,525; 6,190,580 and 6,225,466, the entire disclosures of which are incorporated herein by reference. The amount of the photochromic dye or dye mixture may vary depending on the desired photochromic effect, but typically will amount to from 0.0001 to 1, preferably 0.0001 to 0.1, and particularly preferably 0.001 to 0.1, part by weight per 100 parts by weight of the core resin. The selection of specific dyes or dye mixtures to be used in any given case will depend on the desired coloration, as well as the desired performance characteristics of the resulting lens, such as darkening rate and/or fade rate, and is considered to be within the skill of the art. A suitable neutral gray photochromic dye mixture is described in U.S. Patent No. 6,373,615, at, for example, column 10, line 50+, the entire disclosure of which is incorporated herein by reference. In one preferred aspect, a resin composition includes 0.05 to 0.06%, more preferably 0.056%, photochromic dye mixture by weight of the core resin composition, including 380 to 460 ppm, more preferably 423 ppm, spiro-9-floureno-13'-(6-methoxy-3-(4-N-morpholinyl)phenyl-3-phenyl-indeno[2,1-f]naphtho(1,2-b)pyrane (gray-blue), 40 to 60 ppm, more preferably 46 ppm, of 3-phenyl-3'-(4-N-piperidinyl)-phenyl-6-N-morpholinyl-3H-naphtho[2,1-b]pyrane (ruby), 45 to 65 ppm, more preferably 54 ppm, of 3-phenyl-3'-(4-N-morpholinyl)-phenyl-6-N-morpholinyl-3H-naphtho[2,1-b]pyrane (orange), and 30 to 50 ppm, more preferably 38 ppm, of 3-phenyl-3'-(4-methoxy)-phenyl-6-N-morpholinyl-3H-naphtho[2,1-b]pyrane (yellow).

To form a radiation curable synthetic resin composition according to the present invention, especially a short wavelength, visible light, radiation curable composition, a suitable photo initiator may be incorporated in the core resin composition. Typically the resin composition will include from 0.01 to 3, and preferably 0.02 to 1, part by weight of photo initiator per 100 parts by weight of the core resin. Examples of suitable photo initiators include benzophenone, 2,2-dimethoxy-2-phenyl acetophenone, 1-hydroxycyclohexyl phenyl ketone, 2-methyl-1-[4-(methylthio)phenyl]-2-morpholino propan-1-one, 2-hydroxy-2-methyl-1-phenylpropan-1-one, bis(2,6-dimethoxybenzoyl)-2,4,4-trimethylpentyl phosphine oxide, 2,4,6-trimethylbenzoyl diphenylphosphine oxide, bis(2,4,6-trimethylbenzoyl)-phenylphosphine oxide and mixtures thereof. Preferred photo initiators include

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2,4,6-trimethylbenzoyl diphenylphosphine oxide, bis(2,4,6-trimethylbenzoyl)-phenylphosphine oxide, or mixtures thereof.

If desired, a thermal polymerization initiator may also be incorporated in the synthetic resin composition to facilitate use of thermal curing or combination radiation/thermal curing process techniques. For example, the resin composition may advantageously contain from 0.01 to 3, and preferably 0.02 to 1, part by weight of a thermal initiator per 100 parts by weight of the core resin. Examples of suitable thermal initiators include t-amyl peroxy-2-ethylhexanoate, t-butyl peroxy-2-ethylhexanoate, t-butyl peroxy-2-methylbenzoate, 1,1-di-(t-butylperoxy)-3,3,5-trimethylcyclohexane, t-butyl peroxy-3,5,5-trimethylhexanoate, t-butyl peroxy 2-ethylhexyl carbonate, dibenzoyl peroxide, t-amyl peroxy benzoate, 2,2'-azobis(2,4-dimethylpentanenitrile), 2,2'-azobis(2-methylpropanenitrile), 2,2'-azobis(2-methylbutanenitrile), 1,1'-azobis(cyclohexane-carbonitrile), and mixtures thereof. Particularly preferred thermal initiators include 2,2'-azobis(2,4-dimethylpentanenitrile), 2,2'-azobis(2-methylpropanenitrile), 2,2'-azobis(2-methylbutanenitrile), 1,1'-azobis(cyclohexanecarbonitrile), or mixtures thereof.

In one preferred aspect, the resin composition comprises an initiator mixture comprising both a photo initiator and a thermal initiator. Castable resin compositions according to the invention desirably will have a viscosity of less than 400 cps at room temperature.

The curable synthetic resin composition of the present invention may also comprise up to 5 parts by weight of other additives, such as light stabilizers, mold release agents and/or other processing agents, per 100 parts by weight of the core resin composition. For example a benzophenone UV absorber, such as 2-hydroxy-4-methoxybenzophenone, may be included in the resin composition in an amount from about 50 ppm to about 1,000 ppm, preferably from about 100 ppm to about 500 ppm. In one preferred aspect, a resin composition includes 0.019% 2-hydroxy-4-methoxybenzophenone and 0.056% photochromic dye mixture by weight of the core resin composition. One effective processing agent is isopropylxanthic disulfide, which extends pot life and minimizes yellowing of the resin. Pot life is the time

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from when a resin batch is prepared until the last acceptable lens can be produced from that particular batch. In manufacturing photochromic resins, the possibility of yellowness increases after initiators are mixed with the resins, thus the ability to extend pot life is a useful benefit.

The present invention also relates to a radiation cure process in which a mold assembly is filled with a curable synthetic resin composition of the present invention as described above and the filled mold assembly is subjected to a source of actinic radiation. Desirably the radiation source is a filtered actinic radiation source having a primary output at or above the cutoff wavelength of the filter. Where the synthetic resin composition is intended to produce a photochromic article and contains a photochromic dye which is activated at certain visible wavelengths, e.g. wavelengths above 400 nm, it is advantageous to use a filter to cut off substantially all (e.g., 99% or more) of the radiation up to the wavelength where the photochromic dye is active, so that the photochromic dye will not be activated or darkened during the curing process.

The radiation curing process may comprise either a single stage cure up to 30 minutes in length or a multiple stage cure comprising a plurality of stages from 10 seconds to 20 minutes in duration. The use of the multiple stage procedure is advantageous in order to facilitate control of the rate of reaction and the temperature of the resin during curing depending on the type of lenses being processed. It is also desirable to have adequate cooling time and cooling media at the end of each radiation stage to further control the rate of cure and the temperature of the resin. Suitable cooling media include ambient air, chilled air, ambient water and/or chilled water. The multiple stage radiation and cooling process permits rapid effective curing while keeping the temperature of the lens material below the temperature where thermal polymerization of the resin becomes uncontrollable and the reaction autoaccelerates. This maximizes the yield of the process, optimizing optical, physical, and photochromic properties of the cured article.

In one preferred aspect, after the radiation cure it is desirable to have a thermal anneal at a temperature of 50 to 150°C for up to 2 hours. While various thermal

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curing processes are suitable subsequent to the radiation exposure process described above, the following temperature profile has provided acceptable results. After a radiated lens is placed in the oven, the oven temperature is maintained at 60°C for 15 minutes; the temperature is then raised at a rate of 3.3°C/minute to 76°C and is maintained at 76°C for 10 minutes. The temperature is then raised at a rate of 3.3°C/minute to 100°C and is maintained at 100°C for 35 minutes. Thereafter, the temperature of the oven is allowed to cool to room temperature. The thermal annealing may be carried out prior to and/or after removing the plastic lens from the mold assembly in which it is formed.

The present invention also relates to an article, especially a photochromic article, made by molding and curing a synthetic resin composition according to the present invention as described above.

The following table describes a number of methods for producing lenses with acceptable optical, physical, and photochromic performance when cast using the formulation(s) as described above.

Table 1 Methods for producing lenses

Cure Example	Description
1	Using 420 nm peak output low pressure Hg lamps spaced three to six inches apart and GG420 glass as a filter, expose both sides of the lens or article for 20 minutes. Following the radiation exposure, the articles were put into an oven at 120°C for 25 to 30 minutes.
2	Using 420 nm peak output low pressure Hg lamps spaced three to six inches apart and GG420 glass as a filter, expose both sides of the lens or article for 2.75 to 3 minutes. After this initial exposure, the gasket was removed from the article and exposed to the actinic light for an additional 9 minutes. Following the radiation exposure, the articles were put into an oven at 80°C for 25 to 30 minutes.
3	Using 420 nm peak output low pressure Hg lamps spaced three to six inches apart and GG420 glass as a filter, both sides of the lens or article were exposed for 12 minutes continuously. Following the radiation exposure, the articles were put into an oven at 70 to 90°C for 30 to 60 minutes.
4	Using 420 nm peak fluorescent tubes spaced three to seven inches apart as well as GG420 glass placed between the lamps and the lens/article being cured, lenses were cured as follows. Lenses were placed on a conveyor belt with 3 curing zones and 2 cooling zones. The exposure consisted of an initial 2.75-minute actinic light exposure followed by a 1.25 minutes period out of the light with an ambient temperature of 55°F to 75°F. This was repeated and then followed by another 2.75 minute exposure and quenching into 20°C water for 2 minutes. After the final portion of the radiation exposure process, lenses were placed in an oven 45 to 90 minutes at temperatures between 60 and 100°C.
5	Using 420 nm peak fluorescent tubes spaced three to seven inches apart as well as GG420 glass placed between the lamps and the lens/article being cured, lenses were cured as follows. The exposure consisted of an initial 2.75-minute actinic light exposure followed by a 1.25 minutes period out of the light. This was repeated and then followed by another 2.75 minute exposure and quenching into 20°C water for 2 minutes. After the final portion of the radiation exposure process, lenses were placed in an oven 45 to 90 minutes at temperatures between 60 and 100°C.

6	Using 420 nm peak fluorescent tubes spaced three to seven inches apart as well as GG420 glass placed between the lamps and the lens/article being cured, lenses were cured as follows. The exposure consisted of an initial 3 minutes actinic light exposure after which the gasket was removed. The article was then exposed to actinic light two more times for 3.5 minutes each time. Following the actinic light exposure, the lenses were placed in an oven for 1 hour at 60°C, followed by 1 hour at 70°C.
7	Using 420 nm peak output low pressure Hg lamps spaced three to six inches apart and GG420 glass as a filter, expose both sides of the lens or article for 3 minutes continuously. After this initial exposure, lenses were exposed using 420 nm peak fluorescent tubes spaced three to seven inches apart as well as GG420 glass placed between the lamps and the lens/article being cured by continuous exposure from both sides for 7 minutes. Following the radiation exposure, the articles were put into an oven at 70°C for 30 to 60 minutes.
8	Using 420 nm peak fluorescent tubes spaced three to seven inches apart as well as GG420 glass placed between the lamps and the lens/article being cured, lenses were cured as follows. Lenses were placed on a conveyor belt that carries the lenses between the lamps. The method consisted of exposing the lenses for 4.25 minutes twice. After the final portion of the radiation exposure process, lenses were placed in an oven 45 to 90 minutes at temperatures between 60 and 100°C.
9	Using 420 nm peak fluorescent tubes spaced three to seven inches apart as well as GG420 glass placed between the lamps and the lens/article being cured, lenses were cured as follows. Lenses were placed on a conveyor belt and exposed to the actinic light source described for 9 minutes. After the final portion of the radiation exposure process, lenses were placed in an oven 30 to 90 minutes at temperatures between 60 and 100°C.
10	Using 420 nm peak output low pressure Hg lamps spaced three to six inches apart and GG420 glass as a filter, expose both sides of the lens or article for 10 minutes continuously. Following the radiation exposure, the articles were put into an oven at 120°C for 25 to 30 minutes.

11	Using 420 nm peak output low pressure Hg lamps spaced three to six inches apart and GG420 glass as a filter, lenses were exposed from each side separately using shutters to control the exposure time from each side. The reaction was monitored using a thermocouple embedded in the lens so the temperature could be controlled as low as possible. Exposure times were from 30 seconds to 4 minutes per side. Following the radiation exposure, the articles were put into an oven at 60 to 120°C for 20 to 90 minutes.
12	Using 420 nm peak fluorescent tubes spaced three to seven inches apart as well as GG420 glass placed between the lamps and the lens/article being cured, lenses were cured as follows. Lenses were placed on a conveyor belt with 3 curing zones and 2 cooling zones. The exposure consisted of an initial 2.75-minute actinic light exposure followed by a 1.25 minutes period out of the light with an ambient temperature of 55°F to 75°F. This was repeated and then followed by another 2.75 minutes exposure. This whole exposure was repeated and then followed by placing the lens into cool water. After the final portion of the radiation exposure process, lenses were placed in an oven 45 to 90 minutes at temperatures between 60 and 100°C.

The following tables exhibit examples of photochromic compositions, process and physical properties of the resulting cured articles. Examples 1-28 below, employ formula (Ia) where $n = n' = 3$, $R_1-R_4 = CH_3$, $X = C(CH_3)_2$, and $y_1-y_8 = H$; formula (Ib) where $n = n' = 5$, $R_1-R_4 = CH_3$, $X = C(CH_3)_2$, and $y_1-y_8 = H$; Formula (IIa) where $m_{avg} = 9$, R_5 and $R_7 = CH_3$, and $R_6 = H$ (polyethylene glycol 400 dimethacrylate); and Formula (IIb) where $m_{avg} = 4$ to 5, R_5 and $R_7 = CH_3$, and $R_6 = H$ (polyethylene glycol 200 dimethacrylate) in the amounts indicated in the table. Bis(2,4,6-trimethylbenzoyl)-phenylphosphine oxide at 0.04% and 2,2'-azobis(2,4-dimethylpentanenitrile) at 0.05% were used as photo and thermal initiators, respectively, based on 100 parts by weight of core resin. A neutral gray photochromic dye mixture, at 0.073%, and a UV-absorber, 2-hydroxy-4-methoxybenzophenone, at 0.025%, were also employed. Isopropylxanthic disulfide was used at 0.03%, based on 100 parts by weight of core resin, in examples 1-5. During one hour mixing at room temperature with the photochromic dye mixture, nitrogen bubbling was employed, followed by degassing under vacuum for 15 minutes. The dye mixture employed in these examples includes a combination of

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550 ppm spiro-9-floureno-13'-(6-methoxy-3-(4-N-morpholinyl)phenyl-3-phenyl-indeno[2,1-f]naphtho(1,2-b)pyrane (gray-blue), 60 ppm of 3-phenyl-3'-(4-N-piperidinyl)-phenyl-6-N-morpholinyl-3H-naphtho[2,1-b]pyrane (ruby), 70 ppm of 3-phenyl-3'-(4-N-morpholinyl)-phenyl-6-N-morpholinyl-3H-naphtho[2,1-b]pyrane (orange), and 50 ppm of 3-phenyl-3'-(4-methoxy)-phenyl-6-N-morpholinyl-3H-naphtho[2,1-b]pyrane (yellow), which provides a gray photochromic dye blocking visible light. All samples were cured under low pressure Hg lamp with 420 nm peak output for 15 to 20 minutes at an intensity of 2.5 mw/cm² with GG420 filter glass (from Schott), followed by annealing at 120°C for 25 to 30 minutes.

Table: Formulation (by wt) of core resin

Example No.	Formula (Ia)	Formula (Ib)	Formula (IIa)	Formula (IIb)	Styrene	Divinyl Benzene	Dipenta-erythritol Pentaacrylate
1	0	29.3	41.5	0.0	18.0	0.0	11.3
2	10	19.3	41.5	0.0	18.0	0.0	11.3
3	20	9.3	41.5	0.0	18.0	0.0	11.3
4	0	29.3	31.5	10.0	18.0	0.0	11.3
5	0	29.3	21.5	20.0	18.0	0.0	11.3
6	0	39.3	24.0	0.0	18.0	0.0	18.8
7	0	45.3	18.0	0.0	18.0	0.0	18.8
8	0	39.3	18.0	0.0	18.0	0.0	24.8
9	0	39.3	24.0	0.0	0.0	18.0	18.8
10	0	45.3	18.0	0.0	0.0	18.0	18.8
11	0	39.3	18.0	0.0	0.0	18.0	24.8
12	0	39.8	17.0	0.0	15.8	10.8	16.5
13	0	34.5	17.0	0.0	15.8	10.8	21.8
14	0	39.8	17.0	0.0	10.8	15.8	16.5
15	0	34.5	17.0	0.0	10.8	15.8	21.8
16	0	36.3	14.0	0.0	24.4	4.0	21.3
17	0	41.0	14.0	0.0	21.0	7.4	16.6
18	0	30.0	15.6	0.0	24.4	4.0	26.0
19	0	41.0	17.1	0.0	21.4	4.0	16.5
20	0	32.6	17.1	0.0	20.9	5.9	23.5
21	0	36.3	14.0	0.0	17.6	10.8	21.3
22	0	41.0	14.0	0.0	13.2	10.8	21.0
23	0	31.1	24.0	0.0	24.4	4.0	16.5
24	0	31.6	14.0	0.0	17.6	10.8	26.0
25	0	41.0	14.0	0.0	21.0	7.4	16.6
26	0	30.0	24.0	0.0	17.6	10.8	17.6
27	0	36.0	19.0	0.0	17.6	10.8	16.5
28	0	36.0	19.0	0.0	24.4	4.0	16.5

Table 3 Properties of cured photochromic samples

Example No.	Activation	Darkness	Deactivation	Refractive Index	Abbe Value	Flex modulus (kpsi)
	Compared to ColorMatic extra gray*					
1	Slower	similar	Faster	1.5413	41.8	123
2	Slower	similar	Faster	1.5398	40.8	143
3	Slower	lighter	Faster	1.5423	40.5	152
4	Slower	lighter	Faster	1.5436	41.2	167
5	Slower	lighter	Faster	1.5413	41.1	179
6	Similar	similar	Faster	1.5396	41.9	115
7	Similar	similar	Faster	1.5396	42.2	120
8	Similar	darker	Faster	1.5403	41.6	136
9	Faster	darker	Much faster	1.5426	41.1	80
10	Faster	darker	Much faster	1.5461	38.4	79
11	Faster	darker	Much faster	1.5451	39.1	81
12	Faster	darker	Faster	1.5542	38.8	168
13	Faster	darker	Faster	1.5516	38.4	159
14	Faster	darker	Faster	1.5533	38.7	149
15	Faster	darker	Faster	1.5510	38.8	162
16	Slower	lighter	Faster	1.5529	39	195
17	Slower	similar	Faster	1.5522	39	178
18	Similar	similar	Faster	1.5450	41.8	197
19	Similar	similar	Faster	1.5496	38.8	168
20	Faster	darker	Faster	1.5493	39.6	174
21	Faster	similar	Faster	1.5525	39.7	173
22	Faster	darker	Faster	1.5493	39.3	132
23	Similar	similar	Faster	1.5484	40.2	174
24	Faster	Darker	Faster	1.5506	39.9	175
25	Faster	Darker	Faster	1.5532	39.1	195
26	Faster	Darker	Faster	1.5494	39.3	174
27	Faster	Darker	Faster	1.5514	39.4	174
28	Slower	Similar	Faster	1.5493	39.6	191

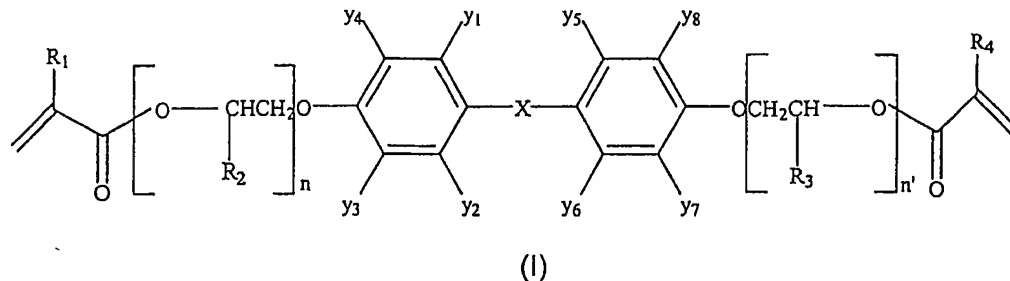
- * ColorMatic extra gray is the best photochromic lenses in over-all properties on the market and is produced by Optische Werke G. Rodenstock located in Munich, Germany. Photochromic properties were obtained after exposure under the natural sun light.

Thicker lenses may also be produced according to the processes of the present invention. Because slower heat transfer rates are associated with thicker lenses, the processing temperatures of the material employed in thicker lens tend to be higher and the selection of thermal initiators may be affected. For example, a useful monomer charge for a typical lens may be 24.37% styrene, 3.99% divinylbenzene, 0.05% 2,2'-azobis(2,4-dimethylpentanenitrile), 0.04% bis(2,4,6-trimethylbenzoyl)-phenylphosphine oxide, 0.20% triphenyl phosphine, 6.29% polyethylene glycol (PEG 400), 36.18% bisphenol A, 21.22% dipentaerythritol pentaacrylate, and 7.67% photochromic dyes. The monomer charge for a similar, but thicker, lens may substitute thermal initiator 1,1'-azobis(cyclohexane-carbonitrile) for 2,2'-azobis(2,4-dimethylpentanenitrile).

The foregoing description and examples have been set forth merely to illustrate the invention and are not intended to be limiting. Since modifications of the described embodiments incorporating the spirit and substance of the invention may occur to persons skilled in the art, the invention should be construed broadly to include all variations falling within the scope of the appended claims and equivalents thereof.

Claims

1. A high refractive index core resin composition comprising
 (i) 2 to 70 parts by weight of at least one first compound corresponding to formula (I):



wherein

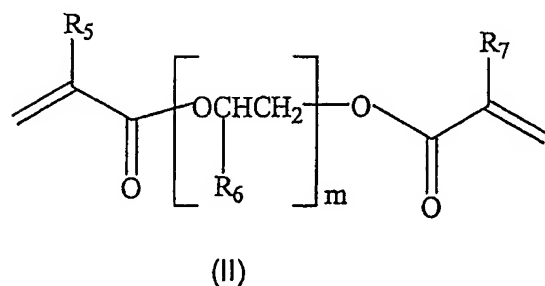
n and n' independently are 0-30,

R₁-R₄ independently represent H or C₁-C₆ alkyl,

X is O, S, SO₂, CO₂, CH₂, CH=CH, C(CH₃)₂ or a single bond, and

y₁-y₈ independently represent H, OH, halogen, mercaptan or C₁-C₄ alkyl,

- (ii) 2 to 80 parts by weight of at least one second compound corresponding to formula (II):



wherein

m is at least 1, and

R₅-R₇ independently represent H or C₁-C₆ alkyl;

- (iii) 2 to 60 parts by weight of a reactive diluent selected from the group consisting of 1,6-hexanediol di(meth)acrylate, trimethylolpropane tri(meth)acrylate, isobornyl (meth)acrylate, 2-hydroxyethyl (meth)acrylate, 2-phenoxyethyl (meth)acrylate, vinyl benzoate, vinyl 4-t-butyl benzoate, styrene, divinyl benzene, and mixtures thereof; and

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(iv) 2 to 60 parts by weight of a multi-functional (meth)acrylate or (meth)acrylate derivative with three or more acrylate functional groups selected from the group consisting of trimethylolpropane tri(meth)acrylate, pentaerythritol tri(meth)acrylate, glyceryl tri(meth)acrylate pentaerythritol tetra(meth)acrylate, di-trimethylolpropane tetra(meth)acrylate, dipentaerythritol penta(meth)acrylate, penta(meth)acrylate ester and mixtures thereof;
per 100 total parts by weight of components (i), (ii), (iii) and (iv).

2. The composition according to claim 1, wherein R_1, R_4, R_5, R_7 are CH_3 , R_2, R_3, R_6 are hydrogen, y_1-y_8 are hydrogen, and X is $C(CH_3)_2$.

3. The composition according to claim 1 or 2, further comprising a mixture of a photo initiator and a thermal initiator.

4. A high refractive index curable photochromic composition comprising:

(a) 100 parts by weight of a core resin mixture according to claim 1;

(b) 0.0001 to 1.0 part by weight of at least one photochromic dye; and

(c) 0.01 to 3 part by weight of a photo initiator;

5. The composition according to claim 4, further comprising (d) 0.01 to 3 part by weight of a thermal initiator.

6. The composition according to claim 4 or 5, further comprising:

(e) up to 5 total parts by weight of other additives selected from the group consisting of light stabilizers, mold release agents and processing agents.

7. The composition according to claim 6, wherein the processing agent comprises isopropylxanthic disulfide.

8. The composition according to anyone of claims 4 to 7, wherein said at least one photochromic dye is selected from the group consisting of chromenes, fulgides, fulgimides, spirooxazines, naphthopyrans, and mixtures thereof.

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9. The composition according to anyone of claims 4 to 8, wherein the composition is radiation curable.
10. The composition according to claim 9, wherein the composition is ultraviolet radiation curable.
11. The composition according to anyone of claims 4 to 10, wherein the photo initiator is selected from the group consisting of benzophenone, 2,2-dimethoxy-2-phenyl acetophenone, 1-hydroxycyclohexyl phenyl ketone, 2-methyl-1-[4-(methylthio)phenyl]-2-morpholino propan-1-one, 2-hydroxy-2-methyl-1-phenylpropan-1-one, bis(2,6-dimethoxybenzoyl)-2,4,4-trimethylpentyl phosphine oxide, 2,4,6-trimethylbenzoyl diphenylphosphine oxide, bis(2,4,6-trimethylbenzoyl)-phenylphosphine oxide, and mixtures thereof.
12. The composition according to claim 11, wherein the photo initiator comprises 2,4,6-trimethylbenzoyl diphenylphosphine oxide, bis(2,4,6-trimethylbenzoyl)-phenylphosphine oxide or mixtures thereof.
13. The composition according to anyone of claims 5 to 12, wherein the thermal initiator is selected from the group consisting of t-amyl peroxy-2-ethylhexanoate, t-butyl peroxy-2-ethylhexanoate, t-butyl peroxy-2-methylbenzoate, 1,1-di-(t-butylperoxy)-3,3,5-trimethylcyclohexane, t-butyl peroxy-3,5,5-trimethylhexanoate, t-butyl peroxy 2-ethylhexyl carbonate, dibenzoyl peroxide, t-amyl peroxy benzoate, 2,2'-azobis(2,4-dimethylpentanenitrile), 2,2'-azobis(2-methylpropanenitrile), 2,2'-azobis(2-methylbutanenitrile), 1,1'-azobis(cyclohexanecarbonitrile), and mixtures thereof.
14. The composition according to claim 13, wherein the thermal initiator comprises 2,2'-azobis(2,4-dimethylpentanenitrile), 2,2'-azobis(2-methylpropanenitrile), 2,2'-azobis(2-methylbutanenitrile), 1,1'-azobis(cyclohexanecarbonitrile) or mixtures thereof.
15. The composition according to anyone of the preceding claims, wherein said

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composition has a viscosity of less than 400 cps at room temperature.

16. A process of producing a cured synthetic resin article comprising:
(i) filling a mold assembly with a synthetic resin composition according to anyone of the preceding claims 1 to 15; and
(ii) curing the resin composition by subjecting the filled mold to radiation from an actinic radiation source.

17. The process according to claim 16, wherein said radiation source is a filtered actinic radiation source.

18. The process according to claim 16 or 17, wherein the filter has a cutoff wavelength at or below the radiation source's primary output wavelength.

19. The process according to claim 16, 17 or 18, wherein the filled mold is subjected to radiation in a single stage radiation exposure step of up to 30 minutes duration.

20. The process according to anyone of claims 16 to 19, wherein the filled mold is subjected to radiation in a multiple stage radiation cure comprising a plurality of radiation exposure steps of from about 10 seconds to about 20 minutes duration each with intervening cooling periods.

21. The process according to claim 20, wherein the intervening cooling is effected by exposing the filled mold at the end of each radiation exposure step to a cooling medium selected from the group consisting of ambient air, chilled air, ambient water and chilled water.

22. The process according to anyone of claims 16 to 21, wherein the synthetic resin composition is subjected to radiation from the actinic radiation source until the composition approaches its thermal polymerization reaction initiation temperature.

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23. The process according to anyone of claims 16 to 22, wherein the curing step further comprises

subjecting the synthetic resin composition to radiation from the actinic radiation source until the composition approaches its thermal polymerization reaction initiation temperature,

cooling the synthetic resin composition,

again subjecting the synthetic resin composition to radiation from the actinic radiation source until the composition approaches its thermal polymerization reaction initiation temperature,

again cooling the synthetic resin composition,

wherein the radiation and cooling steps are repeated until the synthetic resin composition is substantially cured.

24. The process according to anyone of claims 16 to 23, further comprising (iii) thermally annealing the radiation cured composition.

25. The process according to claim 24, wherein the cured composition is thermally annealed at a temperature of from about 50 to about 150°C for up to about 2 hours.

26. The process according to claim 24 or 25, wherein the cured composition is thermally annealed prior to removal from the mold assembly.

27. The process according to claim 24 or 25, wherein the cured composition is thermally annealed after removal from the mold assembly.

28. The process according to claim 24 or 25, wherein thermal annealing is effected both prior to and after removal of the cured composition from the mold assembly.

29. The process according to anyone of claims 16 to 28, wherein a radiation filter, which cuts off 99% of UV radiation up to 400 nm is placed between the radiation source and the photochromic composition so that the photochromic dye is not

activated during the radiation exposure.

30. The process according to anyone of claims 16 to 28, wherein a radiation filter, which cuts off substantially all UV radiation up to a wavelength at which the photochromic dye is not active, is placed between the radiation source and the photochromic composition so that the photochromic dye is not activated during the radiation exposure.

31. A synthetic resin article made from the resin composition according to any one of claims 1 to 15.

32. The synthetic resin article according to claim 31, wherein the resin composition is cured by combined radiation and thermal curing.

33. The synthetic resin article according to claim 31 or 32, wherein the cured resin composition is subjected to thermal annealing.